


Table 5-2 (continued)													
$F_y = 50$ ksi $F_u = 65$ ksi						 L5-L3							
Available Strength in Axial Tension													
Angles													
Shape	Gross Area, $A_g$	Yielding		Rupture, $A_e = 0.75A_g$		Shape	Gross Area, $A_g$	Yielding		Rupture, $A_e = 0.75A_g$			
		kips		kips				kips		kips			
		$P_n / \Omega_t$	$\phi_t P_n$	$P_n / \Omega_t$	$\phi_t P_n$			$P_n / \Omega_t$	$\phi_t P_n$	$P_n / \Omega_t$	$\phi_t P_n$		
		in. <sup>2</sup>	ASD	LRFD	ASD			LRFD	in. <sup>2</sup>	ASD	LRFD	ASD	LRFD
L5×3½×¾	5.85	175	263	143	214	L3½×3½×½	3.25	97.3	146	79.3	119		
	×⅝	4.93	148	222	120		180	×⅞	2.89	86.5	130	70.5	106
	×½	4.00	120	180	97.5		146	×¾	2.50	74.9	113	61.1	91.7
	×⅜	3.05	91.3	137	74.4		112	×⅝	2.10	62.9	94.5	51.4	77.0
	×⅜	2.56	76.6	115	62.4		93.6	×¼	1.70	50.9	76.5	41.6	62.4
	×¼	2.07	62.0	93.2	50.4		75.6	L3½×3×½	3.02	90.4	136	73.8	111
L5×3×½	3.75	112	169	91.3	137	×⅞	2.67		79.9	120	65.0	97.5	
	×⅞	3.31	99.1	149	80.6	121	×¾		2.32	69.5	104	56.6	84.8
	×¾	2.86	85.6	129	69.9	105	×⅝		1.95	58.4	87.8	47.5	71.2
	×⅝	2.41	72.2	108	58.8	88.2	×¼		1.58	47.3	71.1	38.7	58.0
	×¼	1.94	58.1	87.3	47.5	71.2	L3½×2½×½		2.77	82.9	125	67.6	101
	L4×4×¾	5.44	163	245	133	199		×¾	2.12	63.5	95.4	51.7	77.5
×⅝		4.61	138	207	112	169		×⅝	1.79	53.6	80.6	43.6	65.3
×½		3.75	112	169	91.3	137		×¼	1.45	43.4	65.3	35.4	53.1
×⅞		3.30	98.8	149	80.6	121		L3×3×½	2.76	82.6	124	67.3	101
×¾		2.86	85.6	129	69.9	105			×⅞	2.43	72.8	109	59.2
×⅝		2.40	71.9	108	58.5	87.8	×¾		2.11	63.2	95.0	51.4	77.0
×¼	1.93	57.8	86.9	47.1	70.7	×⅝	1.78		53.3	80.1	43.6	65.3	
L4×3½×½	3.50	105	158	85.5	128	×¼	1.44		43.1	64.8	35.1	52.7	
	×¾	2.68	80.2	121	65.3	98.0	×⅜		1.09	32.6	49.1	26.6	39.9
	×⅝	2.25	67.4	101	54.9	82.4	L3×2½×½	2.50	74.9	113	61.1	91.7	
	×¼	1.82	54.5	81.9	44.5	66.8		×⅞	2.22	66.5	99.9	54.3	81.4
	L4×3×⅝	3.99	119	180	97.2	146		×¾	1.93	57.8	86.9	47.1	70.7
		×½	3.25	97.3	146	79.3		119	×⅝	1.63	48.8	73.4	39.7
×¾		2.49	74.6	112	60.8	91.2		×¼	1.32	39.5	59.4	32.2	48.3
×⅝		2.09	62.6	94.1	51.0	76.5		×⅜	1.00	29.9	45.0	24.4	36.6
×¼		1.69	50.6	76.1	41.3	61.9	L3×2×½	2.26	67.7	102	55.3	82.9	
Limit State		ASD	LRFD	Note: Tensile rupture on the effective net area will control over tensile yielding on the gross area unless the tension member is selected so that an end connection can be configured with $A_e \geq 0.923A_g$ .									
	Yielding			$\Omega_t = 1.67$	$\phi_t = 0.90$								
	Rupture			$\Omega_t = 2.00$	$\phi_t = 0.75$								